



1200 New Jersey Ave., SE Washington, D.C. 20590

In Reply Refer To: HSST-1 / CC-151

Mr. Felipe Almanza TrafFix Devices Inc. 160 Avenida La Pata San Clemente CA 92672

Dear Mr. Almanza:

This letter is in response to your October 24, 2018 request for the Federal Highway Administration (FHWA) to review a roadside safety device, hardware, or system for eligibility for reimbursement under the Federal-aid highway program. This FHWA letter of eligibility is assigned FHWA control number CC-151 and is valid until a subsequent letter is issued by FHWA that expressly references this device.

### **Decision**

The following device is eligible within the length-of-need, with details provided in the form which is attached as an integral part of this letter:

SLED to SentryII

### Scope of this Letter

To be found eligible for Federal-aid funding, new roadside safety devices should meet the crash test and evaluation criteria contained in the American Association of State Highway and Transportation Officials' (AASHTO) Manual for Assessing Safety Hardware (MASH). However, the FHWA, the Department of Transportation, and the United States Government do not regulate the manufacture of roadside safety devices. Eligibility for reimbursement under the Federal-aid highway program does not establish approval, certification or endorsement of the device for any particular purpose or use.

This letter is not a determination by the FHWA, the Department of Transportation, or the United States Government that a vehicle crash involving the device will result in any particular outcome, nor is it a guarantee of the in-service performance of this device. Proper manufacturing, installation, and maintenance are required in order for this device to function as tested.

This finding of eligibility is limited to the crashworthiness of the system and does not cover other structural features, nor conformity with the Manual on Uniform Traffic Control Devices.

### Eligibility for Reimbursement

Based solely on a review of crash test results and certifications submitted by the manufacturer, and the crash test laboratory, FHWA agrees that the device described herein meets the crash test and evaluation criteria of the AASHTO's MASH. Therefore, the device is eligible for reimbursement under the Federal-aid highway program if installed under the range of tested conditions.

Name of system: SLED to SentryII

Type of system: Terminal

Test Level: MASH Test Level 3 (TL3)

Testing conducted by: KARCO Date of request: October 25, 2018

FHWA concurs with the recommendation of the accredited crash testing laboratory on the attached form.

### Full Description of the Eligible Device

The device and supporting documentation, including reports of the crash tests or other testing done, videos of any crash testing, and/or drawings of the device, are described in the attached form.

### **Notice**

This eligibility letter is issued for the subject device as tested. Modifications made to the device are not covered by this letter. Any modifications to this device should be submitted to the user (i.e., state DOT) as per their requirements.

You are expected to supply potential users with sufficient information on design, installation and maintenance requirements to ensure proper performance.

You are expected to certify to potential users that the hardware furnished has the same chemistry, mechanical properties, and geometry as that submitted for review, and that it will meet the test and evaluation criteria of AASHTO's MASH.

Issuance of this letter does not convey property rights of any sort or any exclusive privilege. This letter is based on the premise that information and reports submitted by you are accurate and correct. We reserve the right to modify or revoke this letter if: (1) there are any inaccuracies in the information submitted in support of your request for this letter, (2) the qualification testing was flawed, (3) in-service performance or other information reveals safety problems, (4) the system is significantly different from the version that was crash tested, or (5) any other information indicates that the letter was issued in error or otherwise does not reflect full and complete information about the crashworthiness of the system.

### **Standard Provisions**

- To prevent misunderstanding by others, this letter of eligibility designated as FHWA
  control number CC-151 shall not be reproduced except in full. This letter and the test
  documentation upon which it is based are public information. All such letters and
  documentation may be reviewed upon request.
- This letter shall not be construed as authorization or consent by the FHWA to use, manufacture, or sell any patented system for which the applicant is not the patent holder.
- This FHWA eligibility letter is not an expression of any Agency view, position, or determination of validity, scope, or ownership of any intellectual property rights to a specific device or design. Further, this letter does not impute any distribution or licensing rights to the requester. This FHWA eligibility letter determination is made based solely on the crash-testing information submitted by the requester. The FHWA reserves the right to review and revoke an earlier eligibility determination after receipt of subsequent information related to crash testing.
- If the subject device is a patented product it may be considered to be proprietary. If proprietary systems are specified by a highway agency for use on Federal-aid projects: (a) they must be supplied through competitive bidding with equally suitable unpatented items; (b) the highway agency must certify that they are essential for synchronization with the existing highway facilities or that no equally suitable alternative exists; or (c) they must be used for research or for a distinctive type of construction on relatively short sections of road for experimental purposes. Our regulations concerning proprietary products are contained in Title 23, Code of Federal Regulations, Section 635.411.

Sincerely,

Michael S. Griffith

Director, Office of Safety Technologies

Michael S. Fuffith

Office of Safety

Enclosures

111

### Request for Federal Aid Reimbursement Eligibility of Highway Safety Hardware

	Date of Request:	October 24, 2018		
	Name:	Felipe Almanza		
ig.	Company:	TrafFix Devices Inc.		
Submitter	Address:	160 Avenida La Pata San Clemente CA 92673		
S	Country:	United States		
	То:	Michael S. Griffith, Director FHWA, Office of Safety Technologies		

I request the following devices be considered eligible for reimbursement under the Federal-aid highway program.

Device & Testing Criterion - Enter from right to left starting with Test Level

			1-1-1	
System Type	Submission Type	Device Name / Variant	Testing Criterion	Test Level
'CC': Crash Cushions, Attenuators, & Terminals	Physical Crash Testing Engineering Analysis	SLED to Sentry II	AASHTO MASH	TL3

By submitting this request for review and evaluation by the Federal Highway Administration, I certify that the product(s) was (were) tested in conformity with the AASHTO Manual for Assessing Safety Hardware and that the evaluation results meet the appropriate evaluation criteria in the MASH.

### Individual or Organization responsible for the product:

Contact Name:	Felipe Almanza	Same as Submitter 🔀
Company Name:	TrafFix Devices Inc.	Same as Submitter 🔀
Address:	160 Avenida La Pata San Clemente CA 92673	Same as Submitter 🔀
Country:	United States	Same as Submitter 🔀
Eligibility Process	isclosures of financial interests as required by the F s for Safety Hardware Devices' document.	Trovi i caci ai Ma Neilibaiseilleik
Eligibility Process	s for Safety Hardware Devices' document. and Karco Engineering LLC share no financial interest	
includes no shared	financial interest but not limited to:	or garing donor in the
i. Compensation i	ncluding wages, salaries, commissions, professional fee	es, or fees for business referrals
iii. Research fundir	ng or other forms of research support;	•
iv. Patents, copyrig	this, licenses, and other intellectual property interests;	
	ship and investment interests;	

### PRODUCT DESCRIPTION

<u>_</u>	New Hardware or	_ Modification to
(*	New Hardware or Significant Modification	Existing Hardware

The SLED is a, non-redirective, gating crash cushion, designed to shield the end of Sentry II Water Cable Barrier (WCB). The SLED is free standing, does not require anchoring to the road surface and can be used on concrete, asphalt, gravel, and dirt surfaces. The surface used for these tests was concrete. The SLED system consists of two main components: one empty yellow Module and one Containment Impact Sled (CIS). The SLED has overall dimensions of aprox. 88.0 in (2.2 m) length X 27.25 in (0.7 m) wide X 45.875 in (1.2 m) tall. The empty yellow module has overall dimensions of approximately 75.75 in (1.9 m) long (pin to pin) X 22.5 in (0.6 m) wide X 45.875 in (1.2 m) tall. The empty yellow module is manufactured from polyethylene that is UV stabilized. A TL-3 SLED end treatment system for shielding the end of Sentry II WCB consists of one empty yellow module connected to the steel CIS. The empty yellow module with the CIS weighs approx. 322 lbs. (146 kg). Permanently molded within the SLED and Sentry II plastic modules are four corrosion resistant cables. The SLED is designed to shield the end of Sentry II WCB of unlimited length with a minimum Length of Need (LON) of 15 connected Sentry II water filled barrier modules.

The connection between the yellow SLED module and the orange or white Sentry II WCB modules is the same as that between the Sentry II WCB modules. The modules have a series of eleven mating knuckles with vertically aligned concentric holes into which, a steel t-pin is inserted. This provides a positive connection between the SLED and Sentry II WCB. The empty yellow SLED module is positioned inside the CIS and is positively connected to it with a steel t-pin. The yellow SLED empty module is visually identical to the Sentry II barrier modules. The yellow SLED module contains drain holes added to prevent the module from being filled. The CIS is designed using a steel tube frame and sheet metal construction. The CIS has overall dimensions of approx. 88 in (2.2 m) long X 27.25 in (0.7 m) wide X 30.5 in (0.77 m) tall and weighs approx.197 lbs (89.9 kg). Bolted to the front impact face on the CIS is the directional indicator panel. The directional indicator panel is a square sheet of plastic that contains directional sheeting on both sides. This allows the user to convert the panel to the proper direction when installing the SLED. Other directional sheeting types and colors are available. The directional indicator panel contours to the curved shape on the front impact face on the CIS and is secured by six bolts. The MASH tested and passed SLED TL-3 end treatment, described above, is used in concert with the MASH Sentry II Water Cable Barrier and the NCHRP-350 Sentry as described within the FHWA Eligibility Letter B-130 and B-279. The MASH tested and passed SLED TL-3 described above is the same product as the previously tested and passed NCHRP-350 SLED TL-3 crash cushion criteria (Reference CC-114). The design manufacturing process, installation is identical between the MASH and NCHRP-350 tested products. Existing inventory is interchangeable as no design changes have been made since the inception of the SLED in February 2011,

### CRASH TESTING

By signature below, the Engineer affiliated with the testing laboratory, agrees in support of this submission that all of the critical and relevant crash tests for this device listed above were conducted to meet the MASH test criteria. The Engineer has determined that no other crash tests are necessary to determine the device meets the MASH criteria.

Engineer Name:	Robert Ramirez		
Engineer Signature:	Robert Ramirez	Otgitally signed by Robe DN: cn=Robert Ramirez, email=rramirez@karco.co Date: 2018,10,18 09:20:0	o=KARCO Engineering, ou=Project Engineer, om. c=US
Address:	9270 Holly Rd. Adelanto, CA 92301		Same as Submitter
Country:	United States		Same as Submitter [

A brief description of each crash test and its result:

	Y	
Required Test Number	Narrative Description	Evaluation Results
3-30 (1100C)	Not applicable for non-redirective crash cushion	Non-Relevant Test, not conducted
3-31 (2270P)	Not applicable for non-redirective crash cushion	Non-Relevant Test, not conducted
3-32 (1100C)	Not applicable for non-redirective crash cushion	Non-Relevant Test, not conducted
3-33 (2270P)	Not applicable for non-redirective crash cushion	Non-Relevant Test, not conducted
3-34 (1100C)	Not applicable for non-redirective crash cushion	Non-Relevant Test, not conducted
3-35 (2270P)	Not applicable for non-redirective crash cushion	Non-Relevant Test, not conducted
3-36 (2270P)	Not applicable for non-redirective crash cushion	Non-Relevant Test, not conducted
3-37 (2270P)	Not applicable for non-redirective crash cushion	Non-Relevant Test, not conducted
3-38 (1500A)	Not applicable for non-redirective crash cushion	Non-Relevant Test, not conducted

		Page 4 of 9
Required Test	Narrative	Evaluation
Number	Description	Results
	The SLED was positioned offset a quarter of	
	the vehicle's width toward the passenger	
	side. The offset position examines the risk of	
	exceeding occupant risk values, vehicle	M.
	instability, and vehicle yaw movement. The	
	test was conducted using a commercially	
	available 2013 Kia Rio 4-door sedan with a	
	test inertial mass of 2,421.7 lbs (1,098.5 kg).	
	The test vehicle impacted the SLED at a	4
	velocity of 64.99 mph (104.59 km/hr) and at	
	an impact angle of 0.6°. The test vehicle	
	impacted the steel Containment Impact	
	Sled (CIS), pushing it downstream crushing	
	and rupturing the yellow empty module	
	within the CIS. As the vehicle continued	
	downstream the adjacent water filled	
	orange and white Sentry II barrier modules	5
	were crushed and ruptured, dispersing the	
	contained water. The vehicle rotated in a	
3-40 (1100C)	clockwise direction about its yaw axis	PASS
	before coming to a controlled stop 51.8 ft	
	(15.8 m) forward and 23.6 ft (7.2 m) laterally	
	from the initial point of impact. The yellow	
	SLED module and orange/white barrier	
	Sentry II modules remained tethered	
	together via the steel t-pin between the	
	module knuckles which connects directly to	
	the internal molded in steel cables. The	
	impacting vehicle was brought to a	
	controlled stop, remained upright, and did	
	not exhibit vaulting throughout the impact	
	event. The test vehicle's occupant	
	compartment was not penetrated and there	
	was negigible in cab deformation. The	
	maximum roll and pitch angle did not	
	exceed 75° and occupant risk values were	
	within limits per MASH specifications for	
	Occupant Impact Velocity (OIV) and	
	Ridedown Acceleration (RA).	

The SLED was positioned in line with the center of the test vehicle. The inline centered position examines the risk of exceeding occupant risk values, vehicle instability, the SLED's capacity to absorb sufficient impact energy, and the SLED's ability to bring the vehicle to a controlled stop. The test was conducted using a commercially available 2012 Ram 1500 4door pickup truck with a test inertial mass of 4,983.5 lbs (2,260.5 kg). The test vehicle impacted the SLED at a velocity of 62.86 mph (101.17 km/hr) and at an impact angle of 0.1°. The test vehicle impacted the steel Containment Impact Sled (CIS), pushing it downstream crushing and rupturing the empty yellow module within the CIS. As the vehicle continued downstream the adjacent water filled orange and white Sentry II barrier modules were crushed and ruptured dispersing the contained water. The yellow SLED module and orange/white barrier Sentry II modules remained tethered together via the steel t-pin between the module knuckles which connects directly to the internal molded in steel cables. The impacting vehicle was brought to a controlled stop 8.9 ft (2.7 m) forward from the initial point of impact, remained upright, and did not exhibit vaulting throughout the impact event. The test vehicle's occupant compartment was not penetrated and there was negligible in cab deformation. The maximum roll and pitch angle did not exceed 75° and occupant risk values were within limits per MASH specifications for Occupant Impact Velocity and Ridedown Acceleration.

PASS

3-41 (2270P)

The SLED was positioned at a nominal angle of 5° with the center of the test vehicle. The angle position examines the risk of exceeding occupant risk values, vehicle instability, capacity to absorb sufficient impact energy, and the SLED's ability to bring the vehicle to a controlled stop. The test was conducted using a commercially available 2013 Kia Rio 4-door sedan with a test inertial mass of 2,433.9 lbs (1,104.0 kg). The test vehicle impacted the crash cushion at a velocity of 60.19 mph (96.86 km/hr) and at an impact angle of 5.4°. The test vehicle impacted the steel Containment Impact Sled (CIS), pushing it rearward crushing and rupturing the empty yellow module within the CIS. As the vehicle continued downstream the adjacent water filled orange and white Sentry II barrier modules were crushed and ruptured, dispersing the contained water. The yellow SLED module and orange/white Sentry II barrier modules remained tethered together via the steel tpin between the module knuckles which connects directly to the internal molded in steel cables. The impacting vehicle was brought to a controlled stop 5.2 ft (1.6 m) forward and 6.6 ft (7.1 m) laterally from the initial point of impact, remained upright, and did not exhibit vaulting throughout the impact event. The test vehicle's occupant compartment was not penetrated and there was negligible in cab deformation. The maximum roll and pitch angle did not exceed 75°. Occupant risk values were within limits per MASH specifications for Occupant Impact Velocity and Ridedown Acceleration.

PASS

3-42 (1100C)

The SLED was positioned at a nominal angle of 5° with the center of the test vehicle. The angle position examines the risk of exceeding occupant risk values, vehicle instability, capacity to absorb sufficient impact energy, and the SLED's ability to bring the vehicle to a controlled stop. The test was conducted using a commercially available 2014 Ram 1500 4-door pickup truck with a test inertial mass of 5,000.0 lbs (2,268.0 kg). The test vehicle impacted the crash cushion at a velocity of 65.47 mph (105.36 km/hr) and at an impact angle of 4.8°. The test vehicle impacted the steel Containment Impact Sled (CIS), pushing it rearward crushing and rupturing the empty yellow module within the CIS. As the vehicle continued downstream the adjacent water filled orange and water Sentry II barrier modules were crushed and ruptured dispersing the contained water. The yellow SLED module and orange/white barrier Sentry II modules remained tethered together via the steel t-pin between the module knuckle which connects directly to the internal molded in steel cables. The impacting vehicle was brought to a controlled stop 115.6 ft (35.2 m) forward and 20.5 ft (6.3 m) laterally from the initial point of impact, remained upright, and did not exhibit vaulting throughout the impact event. The test vehicle's occupant compartment was not penetrated and there was negligible in cab deformation. The maximum roll and pitch angle did not exceed 75°. Occupant risk values were within limits per MASH specifications for Occupant Impact Velocity and Ridedown Acceleration.

3-43 (2270P)

PASS

	14-7	rage o UI 9
	The SLED was positioned at a nominal angle	
	of 20° and the centerline of the impacting	
	vehicle was directed at the corner of the	
	adjacent Sentry II water filled barrier	
	module connected to the empty SLED	
	module within the CIS. The side angled	
	impact test is to evaluate the SLED's ability	B
	to safely bring the impacting vehicle to a	
	controlled stop. This angle and barrier	
	intersection directed the test vehicle into	
( <del>v</del>	the front of the steel Containment Impact	
	Sled (CIS) at its CIP as defined in MASH for	
	test procedures for Gating Non-Redirective	
	Crash Cushions. The test was conducted	
	using a commercially available 2012 Ram	
	1500 4-door pickup truck with a test inertial	
	mass of 5,011.0 lbs (2,273.0 kg). The test	* =
	vehicle impacted the crash cushion at a	
	velocity of 62.19 mph (100.08 km/hr) and at	
	an impact angle of 20.9°. The test vehicle	
	made initial contact with the leading edge	
	of the CIS and the empty yellow SLED	
3-44 (2270P)	module. Upon impact the CIS began to	PASS
,	rotate in a counter clockwise direction and	17,03
	began fracturing the empty yellow module	
	within the CIS. As the vehicle continued to	
	move forward, the adjacent orange and	
	white Sentry II barrier modules also rotated	
	in a counterclockwise direction, were	
	crushed, and ruptured dispersing the	
	contained water. The yellow SLED modules	
	and orange/white Sentry barrier modules	
	remained tethered together via the steel	*
	t-pin between the module knuckles which	
	connects directly to the internal molded in	
	steel cables. The impacting vehicle was	
	brought to a controlled stop 100.85 ft	
	(30.74 m) forward and 89.8 ft (27.37 m)	
	laterally from the initial point of impact,	
	remained upright, and did not exhibit	
¥)	vaulting throughout the impact event. The	
	test vehicle's occupant compartment was	
	not penetrated and the deformation limits	
	were not exceeded. The maximum roll and	
	pitch angle did not exceed 75°.	
	The SLED to Sentry II is not a staged crash	
3-45 (1500A)	cushion and therefore, per MASH, the test is	Non-Relevant Test, not conducted
	not required.	

Full Scale Crash Testing was done in compliance with MASH by the following accredited crash test laboratory (cite the laboratory's accreditation status as noted in the crash test reports.):

Laboratory Name:	Applus IDIADA KARCO Engineering		
Laboratory Signature:	AB	Digitally signed by A DN; cn=Alex Beltran email=abeltran skar Date: 2018;10:25 11:	, o=KARCO Engineering, ou=Testing Laboratory, rco.com, c=US
Address:	9270 Holly Rd Adelanto CA 92301		Same as Submitter
Country:	United States	81	Same as Submitter
Accreditation Certificate Number and Dates of current Accreditation period :	TL-371 Valid until July 1, 2019		

Submitter Signature\*: Telipe almongo

**Submit Form** 

### **ATTACHMENTS**

### Attach to this form:

- 1) Additional disclosures of related financial interest as indicated above.
- 2) A copy of the full test report, video, and a Test Data Summary Sheet for each test conducted in support of this request.
- 3) A drawing or drawings of the device(s) that conform to the Task Force-13 Drawing Specifications [Hardware Guide Drawing Standards]. For proprietary products, a single isometric line drawing is usually acceptable to illustrate the product, with detailed specifications, intended use, and contact information provided on the reverse. Additional drawings (not in TF-13 format) showing details that are relevant to understanding the dimensions and performance of the device should also be submitted to facilitate our review.

### FHWA Official Business Only:

Eligibility Letter		
Number	Date	Key Words

### MASH Test 3-40 Summary











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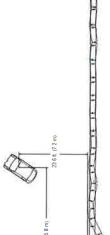
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KARCO Enginearing, LLC.

P36137-01 3-40 11/14/16

KARCO Test No.....

Test Agency..... Test Designation....

General Information

Test Date.....

64.99 mph (104.59 km/h) .0.6°	16.7 in (423 mm) right of vehicle CL	.341.9 kip-ft (463.6 kJ)	N/A  N/A  23.6 ft. (7.2 m) left  None  Satisfactory 6.3°  26.7 8°
Impact Conditions Impact Velocity Impact Angle	Location / Orientation	Kinetic Energy341.9 kip-ft (463.6 kJ)	Exit Conditions  Exit Velocity  Exit Angle  Final Vehicle Position  Vehicle Snagging  Vehicle Pocketing  Vehicle Stability  Maximum Roll Angle  Maximum Pitch Angle  Maximum Yaw Angle  Angle  23.6 ft. (7.2  None  Vehicle Stability  Maximum Pitch Angle  6.3*  Maximum Pitch Angle  25.7 8°

Road Surface.....Concrete

MASH SLED

Test Article
Name / Model.....

Occupant Risk         35.8 ft/s (10.9 m/s)           Lateral OIV         2.6 ft/s (0.8 m/s)           Lateral OIV         2.6 ft/s (0.8 m/s)           Lateral RA         -2.1 g           THIV         36.1 ft/s (11.0 m/s)           PHD         16.6 g           ASI         1.14           Static         13.5 ft (4.1 m)           Dynamic         N/A           Vehicle Damage         12-FD-2           CDC         12FDEV2           CDC         12FDEV2           Maximum Intrusion         0.4 in /10 m/s)
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Figure 2 Summary of Test 3-40

Test Vehicle

### **MASH Test 3-41 Summary**





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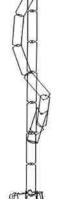


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N/A	N/A	8.9 ft (2.7 m) downstream	2.9 in, (74 mm) left
Exit Conditions Exit Velocity N/A	Exit AngleN/A	Final Vehicle Position	

88.0 in. (2,235 mm)

.... Concrete

Terminal Length.....Road Surface.....

MASH SLED

Name / Model.....

Test Article

11/9/16

Test Date....

Test Agency
KARCO Test No.
Test Designation.

General Information

4.0°	1.3°	4.5°	
dimum Roll Angle49°	cimum Pitch Angle	0.2	
Roll An	Pitch A	ximum Yaw Angle	
dimum	gmum	dimum	

Occupant Risk   Lateral Maximum Intrusion   32.2 ft/s (9.8 m/s)
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Figure 2 Summary of Test 3-41

Year, Make, and Model ..... 2012 RAM 1500

Type / Designation......2270P

Test Vehicle

### **MASH Test 3-42 Summary**













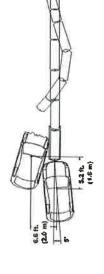
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General Information	imp
Test AgencyKARCO Engineering, LLC.	<u>E</u>
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Name / Model.... Test Article

88.0 in. (2,235 mm) 164.1 ft. (50.0 m) Crash Cushion MASH SLED Concrete Туре..... Installation Length..... Road Surface..... Terminal Length...

Test Vehicle

Curb Mass 2,435.0 lbs (1,104.5 kg)

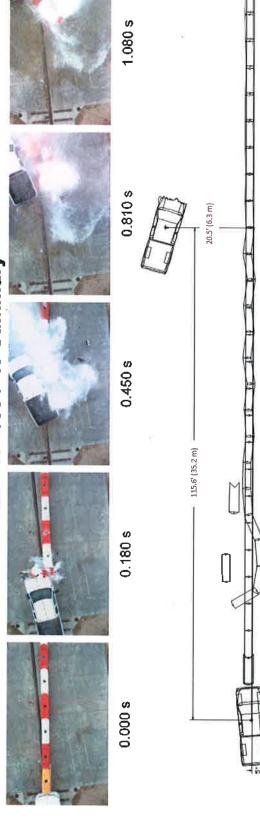
Test Inertial Mass 2,433.9 lbs (1,104.0 kg)
Gross Static Mass 2,595.9 lbs (1,177.5 kg) Year, Make, and Model...... 2013 Kia Rio Type / Designation.....1100C

60.19 mph (96.86 km/h) 5.4° 0.7 in (18 mm) right of vehicle CL 294.8 kip-ft (399.7 kJ)	N/A N/A 5.2 ft (1.6 m) downstream 6.6 ft. (2.0 m) left None Satisfactory 4.2° -2.3°
Impact Conditions Impact Velocity Impact Angle Location / Orientation Kinetic Energy	Exit Conditions  Exit Velocity  Exit Angle  N/A  Final Vehicle Position  6.6 ft.  Vehicle Snagging  None Vehicle Stability  Satisf  Maximum Roll Angle  -2.3°  Maximum Yaw Angle  -2.3°

34.4 ft/s (10.5 m/s) Lateral RA 4.4 g THIV 34.1 ft/s (10.4 m/s) ....... 2.6 ft/s (0.8 m/s) 0.22 in (6 mm) 4.9 ft. (1.5 m) 12FDEW2 Vehicle Damage Scale...... 12-FD-3 .....-17.8 g PHD....16.6 g ASI.....113 CDC.
Maximum Intrusion. Working Width Static Longitudinal OIV..... Lateral OIV..... Test Article Deflections Longitudinal RA... Vehicle Damage Occupant Risk

Figure 2 Summary of Test 3-42

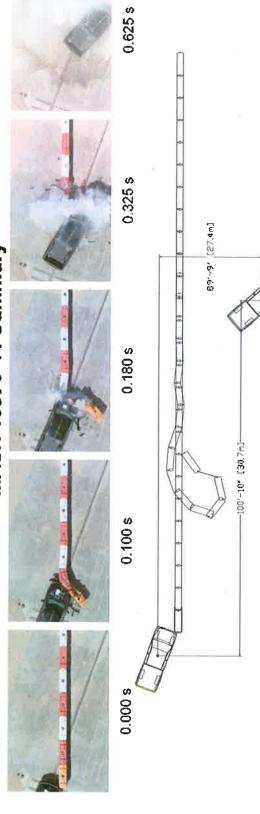
# MASH Test 3-43 Summary



Impact Conditions	Occupant Risk
Impact Velocity 65.47 mph (105.36 km/h)	Longitudinal OfV. 30.8 ft/s (9.4 m/s)
Impact Angle 4.8°	*************
Location / Orientation,	Longitudinal RA6.4 g
ರ	Lateral RA3.4 g
Kinetic Energy 716.4 kip-ft (971.4 kJ)	THIV. 31.2 ft/s (9.5 m/s)
	PHD 6.4 g
Exit Conditions	
Exit Velocity 34.3 mph (55.2 km/h)	
***************************************	Test Article Deflections
Final Vehicle Position 115.6 ft (35.2 m) downstream	Static. 18,8 ft. (5,7 m)
20.5 ft. (6.3 m) left	•
Vehicle SnaggingNone	Working Width7.0 ft. (2.1 m)
Vehicle Pocketing None	
Vehicle StabilitySatisfactory	Vehicle Damage
Maximum Roll Angle4.0°	Vehicle Damage Scale12-FD-4
Maximum Pitch Angle4.9°	CDC 12FDEW3
Maximum Yaw Angle21.0°	-
응은 집 위우 등 및 경험상품이	ntation. osition. ing. ing. y Angle. Angle.

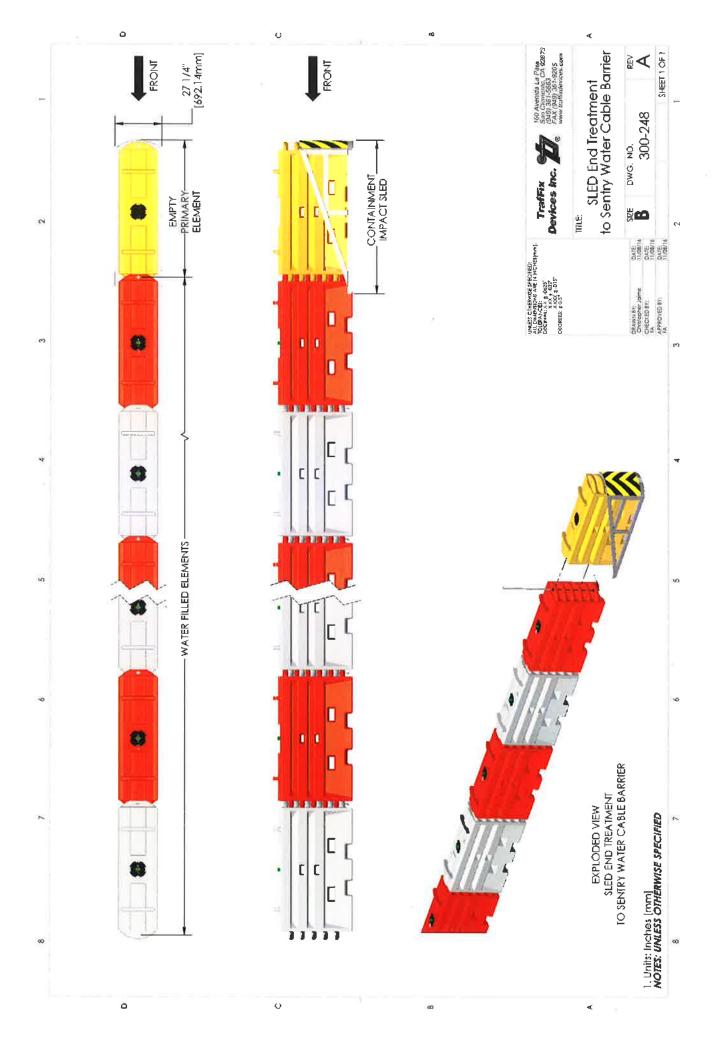
Figure 2 Summary of Test 3-43

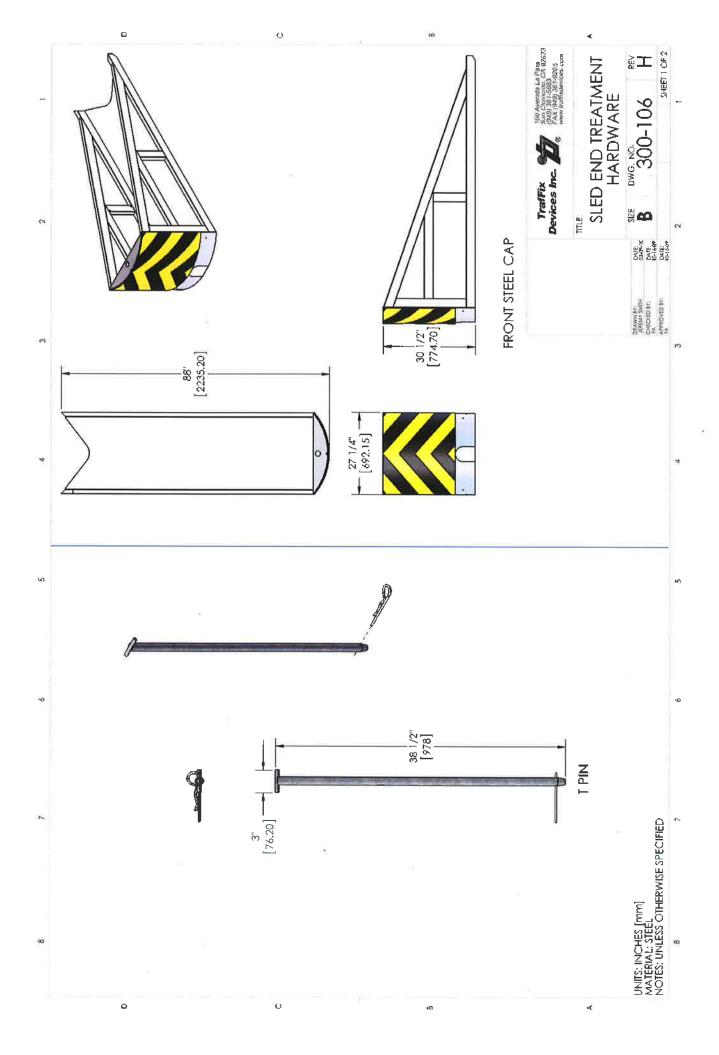
## MASH Test 3-44 Summary

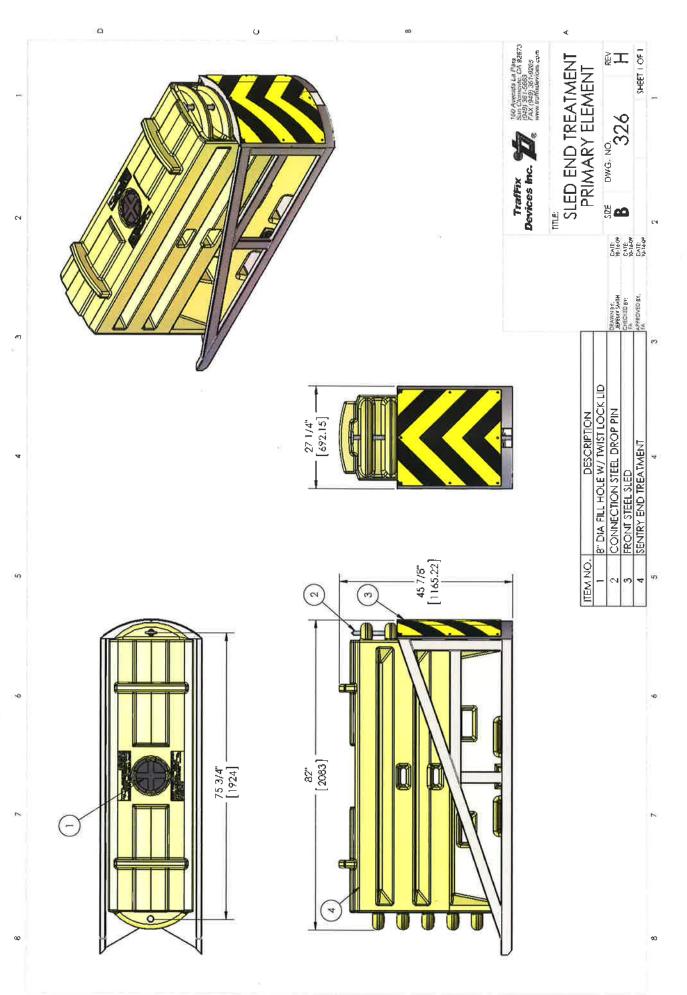


General Information	Impact Conditions	Occupant Risk
Test Agency KARCO Engineering, LLC.	Impact Velocity 62.19 mph (100.08 km/h)	Longitudinal OIV 28.5 ft/s (8.7 m/s)
Test Designation3-44	Location / Orientation 2.4 in. (62 mm) left of the	
Test Date07/28/17	vehicle CL	
	Kinetic Energy 647.9 kip-ft (878.4 kJ)	
Test Article		PHD13a
Name / Model MASH SLED	Exit Conditions	100
Type Crash Cushion	Exit Velocity	
Installation Length162.5 ft. (49.5 m)		Test Article Deflections
Terminal Length88.0 in. (2,235 mm)	Final Vehicle Position 100.85 ft (30.74 m) downstream	Static. 13.9 ft. (4.2 m)
Road SurfaceConcrete	89.80 ft. (27.37 m) right	Dynamic15.4 ft. (4.7 m)
	Vehicle Snagging None	Working Width15.4 ft. (4.7 m)
Test Vehicle	Vehicle Pocketing None	20 September 25 Se
Type / Designation2270P	Vehicle Stability Satisfactory	Vehicle Damage
Year, Make, and Model2012 RAM 1500		Vehicle Damage Scale12-FD-4
Curb Mass4,960.3 lbs (2,250.0 kg)	Maximum Pitch Angle6.7°	
Test Inertial Mass5,011.0 lbs (2,273.0 kg)	Maximum Yaw Angle27.2	·
Gross Static Mass5,011.0 lbs (2,273.0 kg)		L

Figure 2 Summary of Test 3-44







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